



Answer the following questions:

Q1: Complete the following sentences:

- i. is the maximum voltage appearing across the diode in reverse bias.
- ii. The output frequency of a full-wave rectifier with a 60 Hz sinusoidal input is....Hz
- iii. Diode..... add a DC level to an AC voltage.
- iv. If the load resistance of a capacitor filtered full wave rectifier is reduced, the ripple voltages
- v. The DC value of a full wave rectifier voltage with a peak value of 200 is..... .
- vi. The PIV of the bridge rectifier is about.....the value for the center tapped transformer.
- vii. A transistor can be operated as an electronic switch in and.....region.
- viii. The bias methods for discrete BJT circuit are using , , and
- ix. In common base amplifier, the input and output voltages are..... phase.
- x. In common emitter amplifier the gainwith the emitter resistance.
- xi. The maximum current gain is one in the amplifier.
- xii. The maximum voltage gain is one in the amplifier.

Q2: (a) In fig.(1), what is the maximum positive and negative output voltages with $V_i = 20\sin(\omega t)$? Sketch the output waveform. Assume the diode is actual.

(b) The transistor parameters for the circuit in Figure (2) are $\beta_1 = 120$, $\beta_2 = 80$, $V_{BE1(on)} = V_{BE2(on)} = 0.7$ V. Determine the quiescent collector current in each transistor.

Q3: The parameters of the zener diode for the voltage regulator circuit of Fig.(3) are $V_Z = 4.7$ V at test current $I_{ZT} = 53$ mA, $r_Z = 8\Omega$, and $I_{ZK} = 1$ mA. The supply voltage is $V_S = 12 \pm 2$ V, and $R_S = 220\Omega$.

- a) Find the nominal value of the output voltage v_O under no-load condition R_L .
- b) Find the maximum and minimum values of the output voltage for a load resistance of $R_L = 470\Omega$.
- c) Find the nominal value of the output voltage v_O for a load resistance of $R_L = 100\Omega$.
- d) Find the minimum value of R_L for which the zener diode operates in the breakdown region.

Q4: For the amplifier shown in Fig.(4) , $\beta = 80$ and $V_A = 150$ V. (a) Determine the dc voltages at the base and emitter terminals. (b) Using the small signal hybrid π -model calculate the values of R_{in} , R_o , the voltage gain (v_o/v_s) and the current gain $A_i = (i_o/i_s)$.

Q5: The parameters of the amplifier circuit shown in Figure (5) are $V_{CC} = 15$ V, $R_{C1} = R_{C2} = 1$ k Ω , $R_1 = R_3 = 65$ k Ω , $R_2 = R_4 = 25$ k Ω , $R_{E1} = R_{E2} = 400\Omega$, $R_L = 20$ k Ω , and $C_1 = C_2 = C_3 = C_E \approx \infty$. Assume, identical transistors of $\beta = 100$ and $V_A = 100$ V. Calculate the input resistance R_i , the output resistance R_o , and the overall voltage gain $A_v = (v_o/v_s)$.

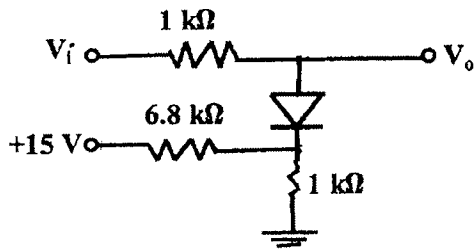


Fig.(1)

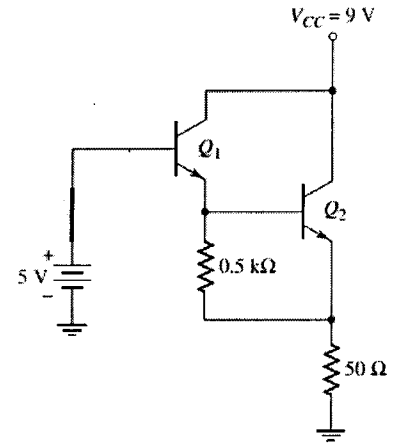


Fig.(2)

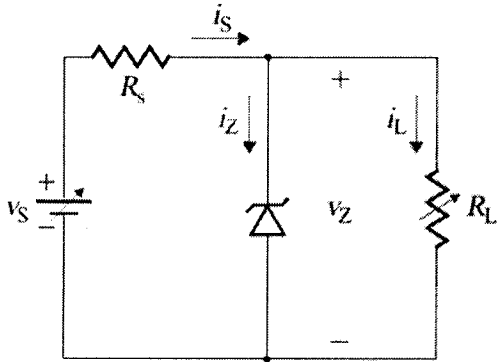


Fig.(3)

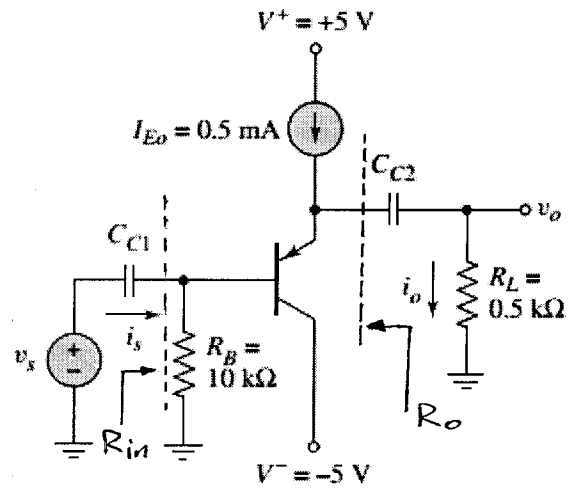


Fig.(4)

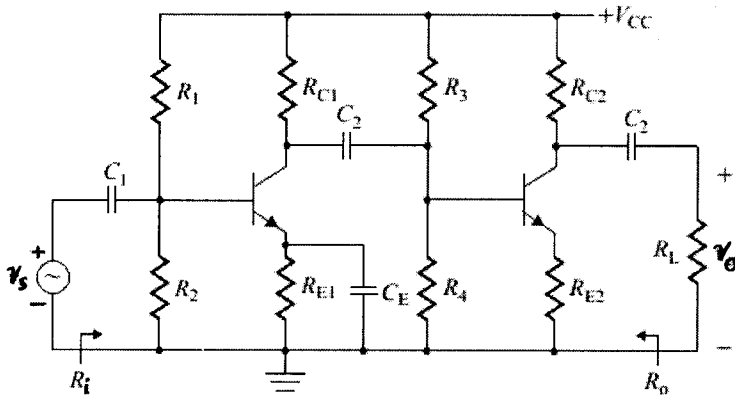


Fig.(5)

BEST WISHES

Hossam Labib



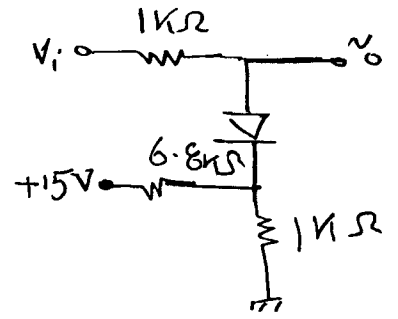
Answer the following questions:

Q1: Complete the following sentences:

- i. PIV is the maximum voltage appearing across the diode in reverse bias.
 - ii. The output frequency of a full-wave rectifier with a 60 Hz sinusoidal input is 120 Hz
 - iii. Diode clampers add a DC level to an AC voltage.
 - iv. If the load resistance of a capacitor filtered full wave rectifier is reduced, the ripple voltages increase.
 - v. The DC value of a full wave rectifier voltage with a peak value of 200 is $(V_{dc}=2*V_m/\pi=400/\pi=127.324V)$.
 - vi. The PIV of the bridge rectifier is about half the value for the center tapped transformer.
 - vii. A transistor can be operated as an electronic switch in cut off and saturation region.
 - viii. The bias methods for discrete BJT circuit are using single power supply (voltage divider bias), using two power supplies ,and using a collector-to- base feedback resistor, OR using constant current source.
 - ix. In common base amplifier, the input and output voltages are in phase.
 - x. In common emitter amplifier the gain decreases with the emitter resistance.
 - xi. The maximum current gain is one in the common base amplifier.
 - xii. The maximum voltage gain is one in the common collector amplifier.
-

Q2:

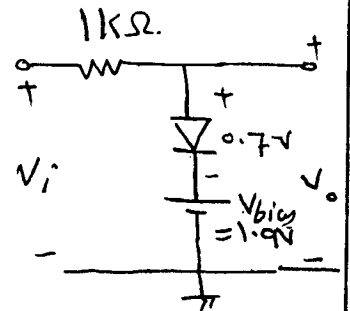
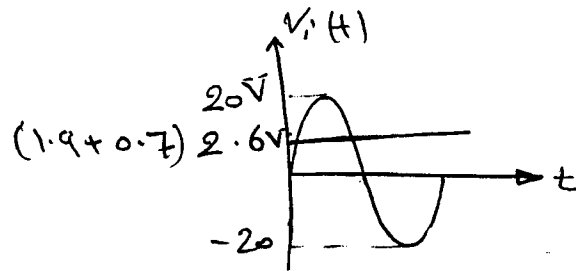
(a) In Fig. shown what is the maximum positive and negative o/p voltages with $V_i = 20 \sin(\omega t)$? Sketch the o/p waveform. Assume the diode is actual.



Solution

$$V_{bias} = \frac{15 \times 1k}{(6.8 + 1)k} = 1.9V \rightarrow \textcircled{2}$$

Then the circuit is +ve biased clipper



For $V_i < 2.6V \Rightarrow$ Diode is off $\Rightarrow V_o = V_i$

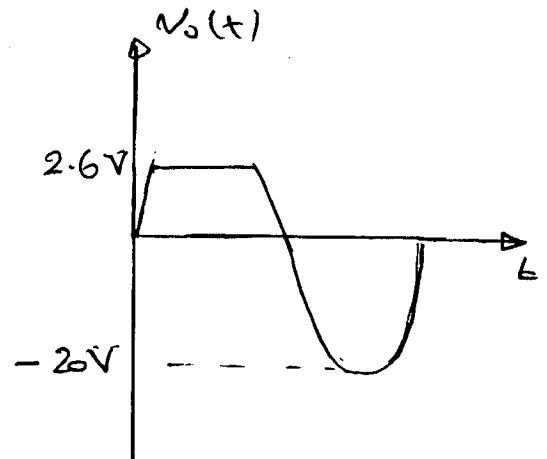
$\rightarrow \textcircled{1}$

For $V_i > 2.6V \Rightarrow$ Diode is on $\Rightarrow V_o = 2.6V$

$$V_o|_{\max_{+ve}} = 2.6V \rightarrow \textcircled{1.5}$$

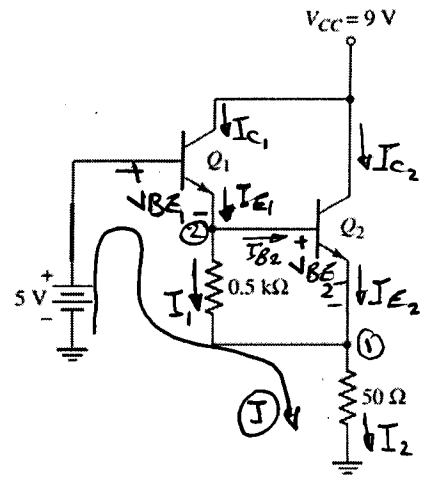
$$V_o|_{\max_{-ve}} = -20V \rightarrow \textcircled{1.5}$$

$\textcircled{2}$



Q2:

- (b) The transistor parameters for the circuit in Figure (2) are $\beta_1 = 120$, $\beta_2 = 80$, $V_{BE1(on)} = V_{BE2(on)} = 0.7$ V. Determine the quiescent collector current in each transistor.



Solution

Loop (I)

$$-5 + V_{BE1} + V_{BE2} + 50 * I_2 = 0$$

$$I_2 = \frac{5 - V_{BE1} - V_{BE2}}{50}$$

$$= \frac{5 - 0.7 - 0.7}{50} = \frac{3.6}{50} = 72 \text{ mA}$$

$$I_1 = \frac{V_{BE2}}{0.5 \text{ K}} = \frac{0.7}{0.5 \text{ K}} = 1.4 \text{ mA}$$

at node ①

$$I_1 + I_{E2} = I_2 \Rightarrow I_{E2} = I_2 - I_1$$

$$I_{E2} = (72 - 1.4) \text{ m} = 70.6 \text{ mA}$$

$$I_{B2} = \frac{I_{E2}}{1 + \beta_2} = \frac{70.6 \text{ m}}{81} = 871.605 \text{ } \mu\text{A}$$

$$I_{C2} = \beta_2 I_{B2} = 871.605 \text{ } \mu\text{A} * 80 = 69.728 \text{ mA}$$

at node ②

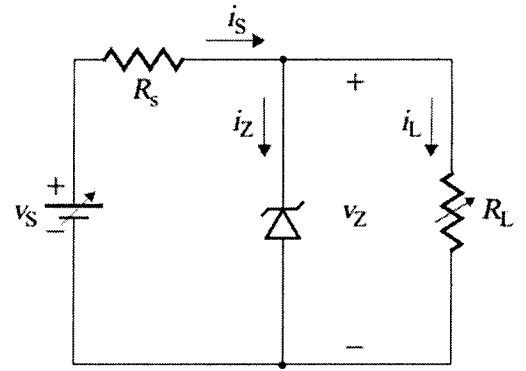
$$I_{E1} = I_{B2} + I_1 = 871.605 \text{ } \mu\text{A} + 1.4 \text{ m} = 2.272 \text{ mA}$$

$$I_{C1} = \alpha_1 I_{E1} = \frac{\beta_1}{1 + \beta_1} I_{E1}$$

$$= \frac{120}{121} * 2.272 \text{ m} = 2.253 \text{ mA}$$

Q3:

The parameters of the zener diode for the voltage regulator circuit of Fig. () are $V_Z = 4.7 \text{ V}$ at test current $I_{ZT} = 53 \text{ mA}$, $r_Z = 8 \Omega$, and $I_{ZK} = 1 \text{ mA}$. The supply voltage is $V_S = 12 \pm 2 \text{ V}$, and $R_S = 220 \Omega$.



- Find the nominal value of the output voltage v_O under no-load condition R_L .
- Find the maximum and minimum values of the output voltage for a load resistance of $R_L = 470 \Omega$.
- Find the nominal value of the output voltage v_O for a load resistance of $R_L = 100 \Omega$.
- Find the minimum value of R_L for which the zener diode operates in the breakdown region.

Solution

$V_Z = 4.7 \text{ V}$ @ $I_{ZT} = 53 \text{ mA}$; $r_Z = 8 \Omega$

$r_{ZK} = 500 \Omega$ at $I_{ZK} = 1 \text{ mA}$

$V_S = 12 \pm 2 \text{ V}$, and $R_S = 220 \Omega$

1st find V_{Z0}

$\therefore V_Z = V_{Z0} + I_Z r_Z \Rightarrow V_{Z0} = V_Z - I_Z r_Z$

$V_{Z0} = 4.7 - 53 \text{ m} * 8 = 4.28 \text{ V}$

(a) For no load i.e $R_L = \infty$ find v_O at nominal value of $V_S = 12 \text{ V}$

$I_S = I_Z = \frac{V_S - V_{Z0}}{R_S + r_Z} = \frac{12 - 4.28}{220 + 8} = 33.86 \text{ mA}$

$\therefore v_O = V_{Z0} + I_Z r_Z = 4.28 + 33.86 \text{ m} * 8 = 4.55 \text{ V}$

(b) find The max. and min. values of The o/p voltage for $R_L = 470 \Omega$

The max. value $v_{O|max}$ occurs at $V_S|_{max}$

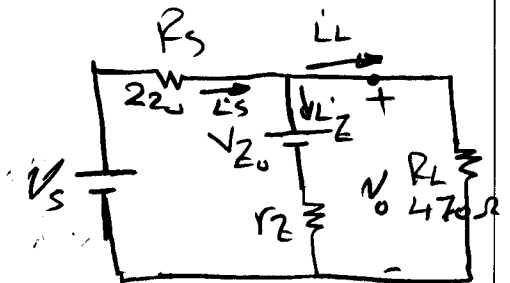
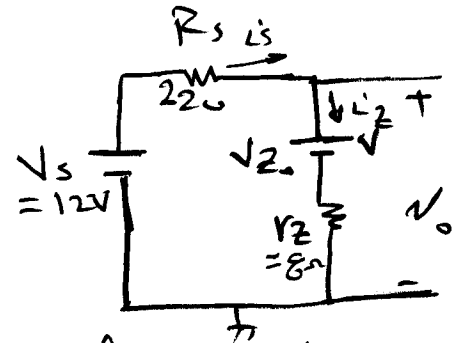
$\therefore V_S|_{max} = V_S + 2 \text{ V} = 12 + 2 = 14 \text{ V}$

-At $V_S = 12 \text{ V}$ (Nominal value) and

$R_L = 470 \Omega$ is connected

$I_L = \frac{V_Z}{R_L} = \frac{4.7}{470} = 10 \text{ mA}$

$I_S = \frac{V_S - V_Z}{R_S} = \frac{12 - 4.7}{220} = 33.2 \text{ mA}$



$$\therefore I_{Z|_{\text{Loaded}}} = I_S - I_L = 33.2 \text{ mA} - 10 \text{ mA} = 23.2 \text{ mA}$$

$$\therefore V_0 = V_{Z_0} + I_{Z|_{\text{L}}} R_Z$$

$$= 4.28 + 23.2 \times 10^{-3} \times 8 = 4.47 \text{ V}$$

For $V_S|_{\text{max}} = 14 \text{ V}$ and $R_L = 470 \Omega$ connected.

$$I_S = \frac{V_S - V_0}{R_S} = \frac{14 - 4.47}{220} = 43.32 \text{ mA}$$

$$I_L = \frac{V_0}{R_L} = \frac{4.47}{470} = 9.51 \text{ mA}$$

$$\therefore I_{Z|_{\text{max}}} = I_S - I_L = 43.32 - 9.51 = 33.81 \text{ mA}$$

$$\therefore V_0|_{\text{max}} = V_{Z_0} + I_{Z|_{\text{max}}} R_Z$$

$$= 4.28 + 33.81 \text{ mA} \times 8 = 4.55 \text{ V}$$

For $V_S|_{\text{min}} = 12 - 2 = 10 \text{ V}$

$$I_S = \frac{V_S - V_0}{R_S} = \frac{10 - 4.47}{220} = 25.14 \text{ mA}$$

$$I_L = \frac{V_0}{R_L} = \frac{4.47}{470} = 9.51 \text{ mA}$$

$$I_{Z|_{\text{min}}} = I_S - I_L = 25.14 - 9.51 = 15.63 \text{ mA}$$

$$\therefore V_0|_{\text{min}} = V_{Z_0} + I_{Z|_{\text{min}}} R_Z = 4.28 + 15.63 \text{ mA} \times 8 = 4.41 \text{ V}$$

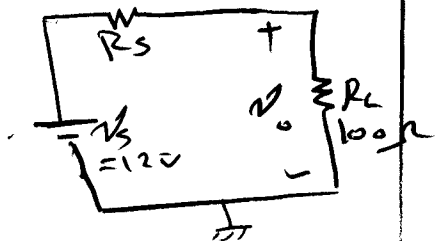
(c) For $R_L = 100$ at nominal value of V_S find V_0

$$\text{For } V_S = 12 \text{ V} \Rightarrow I_L = \frac{V_Z}{R_L} = \frac{4.7}{100} = 47 \text{ mA}$$

$$\therefore I_S = 33.2 \text{ mA} \Rightarrow I_L > I_S \quad (I_S = I_L + I_Z)$$

\therefore Zener must be off

$$\therefore V_0 = \frac{V_S R_L}{R_L + R_S} = \frac{12 \times 100}{100 + 220} = 3.75 \text{ V}$$



(d) Find the min. value of R_L for which the Zener operate in breakdown region

To operate in break down region \Rightarrow Zener current $= I_{ZK}$
 $= 1 \text{ mA} = I_Z = I_{Z \min}$ $V_{ZK} \approx V_{Z0} = V_Z = 4.28 \text{ V}$

$$\therefore I_{S \min} = \frac{V_{S \min} - V_{Z0}}{R_s} = \frac{10 - 4.28}{220} = 26 \text{ mA}$$

$$\therefore I_L = I_{S \min} - I_{Z \min} = 26 \text{ mA} - 1 \text{ mA} = 25 \text{ mA}$$

$\therefore R_{L \min}$ To operate in breakdown region is given by

$$R_L \geq \frac{V_Z}{I_L}$$

$$R_{L \min} \geq \frac{4.28}{25 \text{ m}} = 171.2 \Omega.$$

Q4:

For the amplifier shown in Fig.(4), $\beta = 80$ and $V_A = 150$ V. (a) Determine the dc voltages at the base and emitter terminals. (b) Using the small signal hybrid π -model calculate the values of R_{in} , R_o , the voltage gain (v_o/v_s), and the current gain (I_o/I_s).

Solution

Dc Analysis

$$I_E = I = 0.5 \text{ mA}$$

$$I_B = \frac{I_E}{1+\beta} = \frac{0.5 \text{ mA}}{1+80} = 6.173 \text{ } \mu\text{A}$$

$$I_C = \beta I_E = \frac{\beta}{1+\beta} I_E$$

$$= \frac{80}{81} * 0.5 \text{ mA} = 0.494 \text{ mA}$$

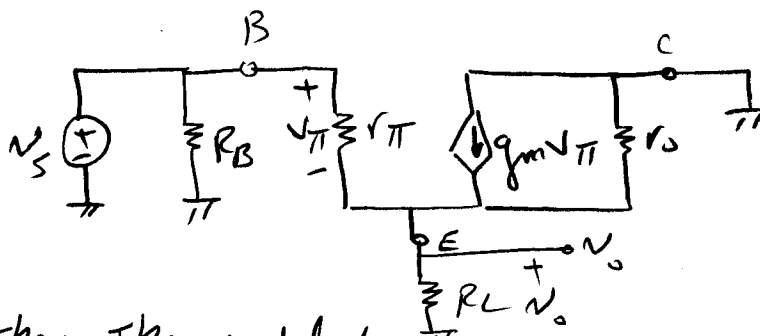
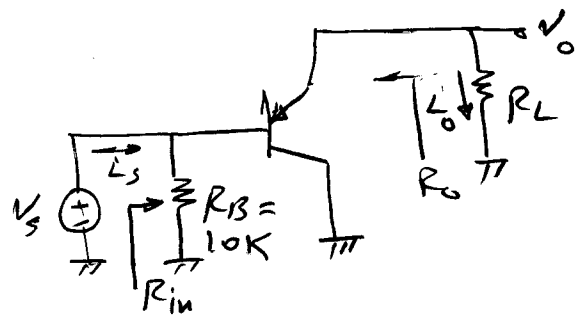
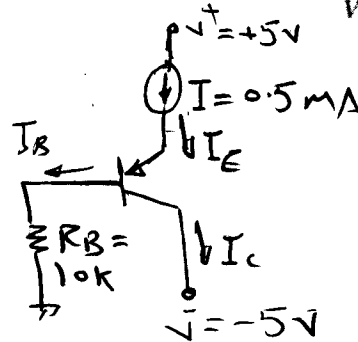
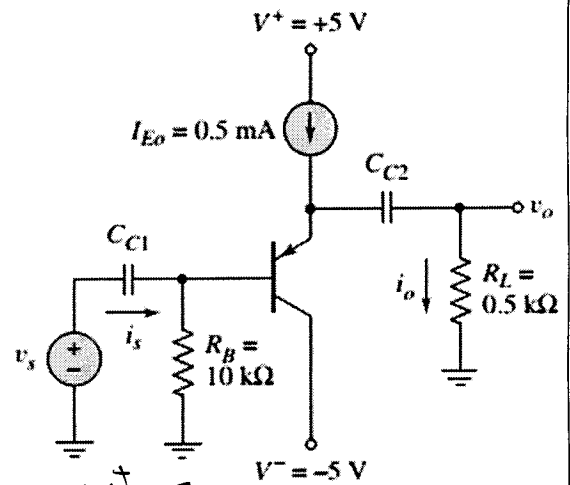
$$g_m = \frac{I_C}{V_T} = \frac{0.494 \text{ m}}{25 \text{ m}} = 19.76 \text{ mA/V}$$

$$r_{\pi} = \frac{\beta}{g_m} = \frac{80}{19.76 \text{ m}} = 4.049 \text{ k}\Omega$$

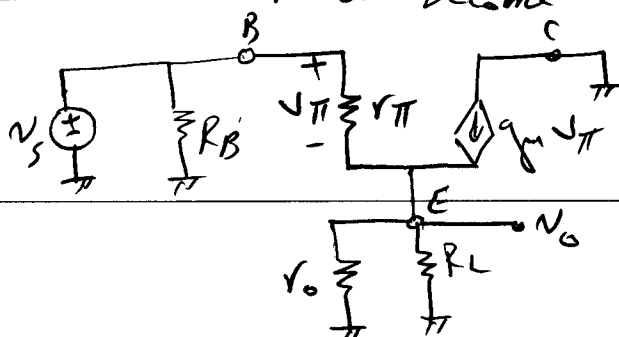
$$r_o = \frac{V_A}{I_C} = \frac{150}{0.494 \text{ m}} = 303.644 \text{ k}\Omega$$

Ac Analysis

Using π -model



if $R_L \parallel R_o$ Then the model become -



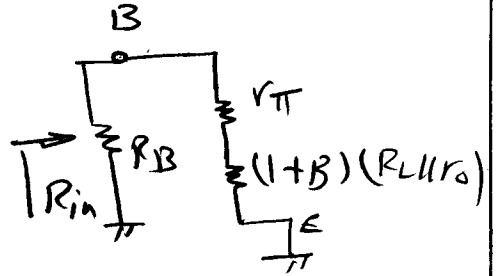
To find R_i

$$R_L || r_o = 0.5K || 303.644K = 499.178\Omega$$

$$R_{in} = R_B || [r_{\pi} + (1+\beta)(R_L || r_o)]$$

$$= 10K || [4.049K\Omega + (1+80)(499.178)]$$

$$= 10K || 44.482K = 8.165 K\Omega$$

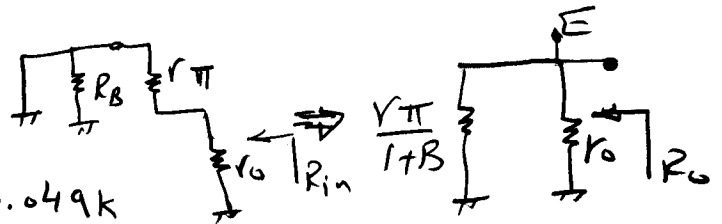


To find R_o

$$R_o | \Rightarrow R_B || s.c = 0$$

$$R_o = r_o || \frac{r_{\pi}}{1+\beta} = 303.644K || \frac{4.049K}{81}$$

$$= 303.644K || 50\Omega \approx 50\Omega$$



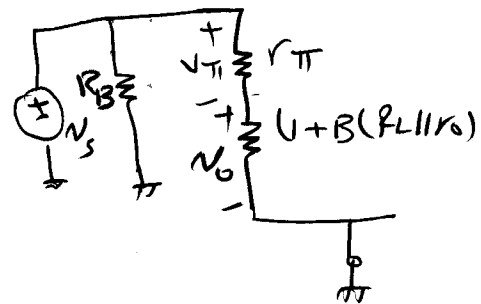
To find $A_v = \frac{V_o}{V_s}$

$$V_o = \frac{V_s (1+\beta)(R_L || r_o)}{r_{\pi} + (1+\beta)(R_L || r_o)}$$

$$\therefore A_v = \frac{V_o}{V_s} = \frac{(1+\beta)(R_L || r_o)}{r_{\pi} + (1+\beta)(R_L || r_o)}$$

$$= \frac{81(499.178)}{4.049K + 81(499.178)}$$

$$= \frac{40.433K}{4.049K + 40.433K} = 0.91 \text{ V/V}$$



To find $A_i = \frac{I_o}{I_s}$

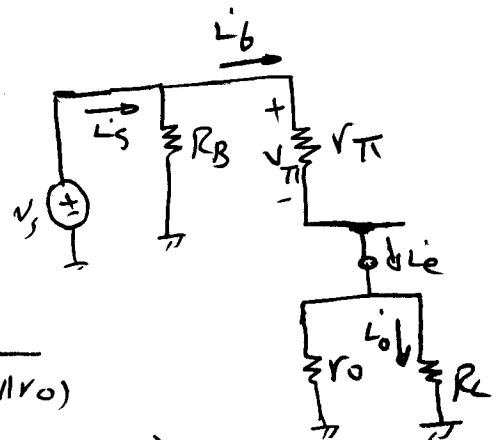
$$I_o = i_e \frac{r_o}{r_o + R_L} = (1+\beta) I_b \frac{r_o}{r_o + R_L}$$

$$I_b = I_s \frac{R_B}{R_B + r_{\pi} + (1+\beta)(R_L || r_o)}$$

$$A_i = \frac{I_o}{I_s} = (1+\beta) \left(\frac{r_o}{r_o + R_L} \right) \left(\frac{R_B}{R_B + r_{\pi} + (1+\beta)(R_L || r_o)} \right)$$

$$= 81 \left(\frac{303.644K}{303.644K + 0.5K} \right) \left(\frac{10K}{10K + 4.049K + 81 \times 499.17} \right)$$

$$= 14.84 \text{ V/V}$$



Q5:

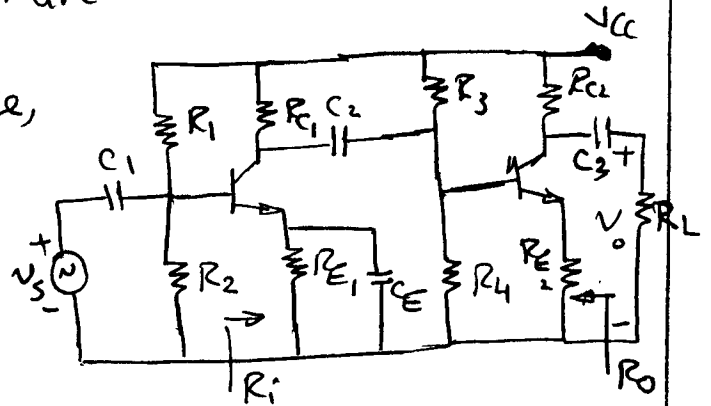
The parameters of the circuit shown are

$V_{CC} = 15\text{ V}$, $R_{C1} = R_{C2} = 1\text{ k}\Omega$,
 $R_1 = R_3 = 65\text{ k}\Omega$, $R_2 = R_4 = 25\text{ k}\Omega$,

$R_{E1} = R_{E2} = 400\ \Omega$; $R_L = 20\text{ k}\Omega$,
 and $C_1 = C_2 = C_3 = C_E = \infty$

Assume, identical transistors of $\beta = 100$ and $V_A = 100\text{ V}$.

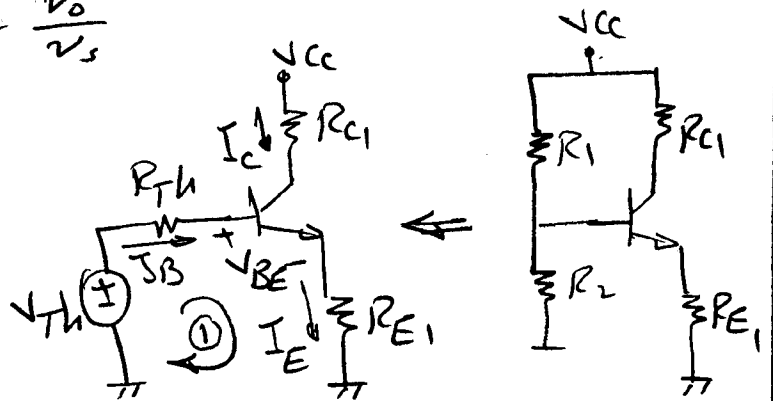
calculate R_i , R_o , and $A_v = \frac{V_o}{V_s}$



Solution

DC Analysis

All cap. o.c
 for Q_1 and Q_2



$R_{TH} = R_1 || R_2 = 65\text{ k} || 25\text{ k} = 18.1\text{ k}\Omega$ \rightarrow ①,
 $V_{TH} = \frac{V_{CC} R_2}{R_1 + R_2} = \frac{15 \times 25\text{ k}}{25\text{ k} + 65\text{ k}} = 4.17\text{ V}$ \rightarrow ①,

Loop ①

$-V_{TH} + I_B R_{TH} + V_{BE} + I_E R_{E1} = 0$ \rightarrow ①

$\therefore I_E = (1 + \beta) I_B$

$I_B (R_{TH} + (1 + \beta) R_{E1}) = V_{TH} - V_{BE}$

$I_B = \frac{V_{TH} - V_{BE}}{R_{TH} + (1 + \beta) R_{E1}} = \frac{4.17 - 0.7}{18.1\text{ k} + 101 \times 400} = 59.32\ \mu\text{A}$ \rightarrow ①

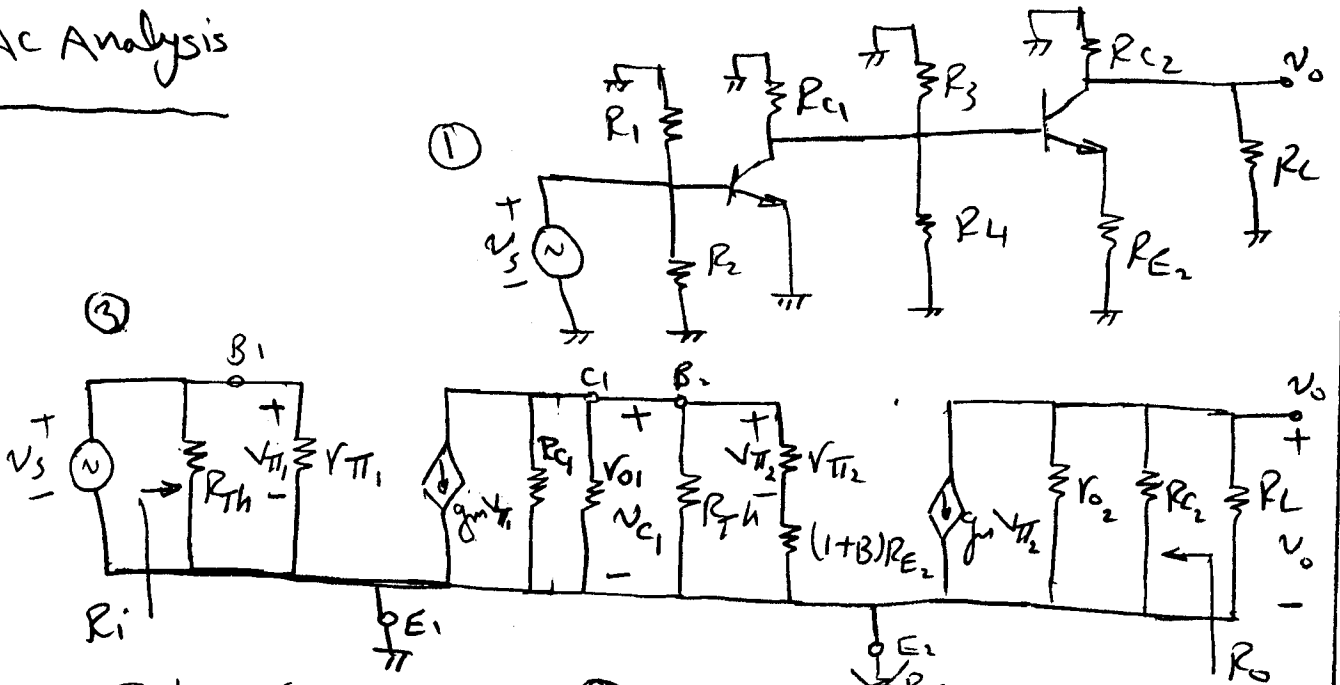
$I_C = \beta I_B = 5.932\text{ mA}$ \rightarrow 0.5

$\therefore g_{m1} = g_{m2} = g_m = \frac{I_C}{V_T} = \frac{5.932\text{ m}}{25\text{ m}} = 237.28\text{ mA/V}$ \rightarrow 0.5

$r_{\pi 1} = r_{\pi 2} = r_{\pi} = \frac{\beta}{g_m} = \frac{100}{237.28 \times 10^3} = 421\ \Omega$ \rightarrow 0.5

$r_{o1} = r_{o2} = r_o = \frac{V_A}{I_C} = \frac{100}{5.932\text{ m}} = 16.86\text{ k}\Omega$ \rightarrow 0.5

AC Analysis



$$R_i = R_{Th} \parallel r_{\pi 1} \longrightarrow \textcircled{1}$$

$$= 18.1 \text{ K} \parallel 421 = 411 \Omega \longrightarrow \textcircled{1}$$

$$R_o = r_{o 2} \parallel R_{c 2} \longrightarrow \textcircled{1}$$

$$v_s = 0 = 16.86 \text{ K} \parallel 1 \text{ K} \Omega = 944 \Omega \longrightarrow \textcircled{1}$$

$$R_{Ley} = r_{o 2} \parallel R_{c 2} \parallel R_L = 16.86 \text{ K} \parallel 1 \text{ K} \parallel 20 \text{ K} = 901.5 \Omega$$

$$R_{eq} = R_{c 1} \parallel r_{o 1} \parallel R_{Th} \parallel [r_{\pi 2} + (1 + \beta) R_{E 2}]$$

$$= 1 \text{ K} \parallel 16.86 \text{ K} \parallel 18.1 \text{ K} \parallel [421 + 101 \times 400]$$

$$= 1 \text{ K} \parallel 16.86 \text{ K} \parallel 18.1 \text{ K} \parallel 40.82 \text{ K} \Omega = 878 \Omega$$

$$v_o = -g_m v_{\pi 2} R_{Ley} \longrightarrow \textcircled{1}$$

$$v_{c 1} = -g_m v_{\pi 1} R_{eq} \longrightarrow \textcircled{1}$$

$$v_{\pi 2} = v_{c 1} \frac{r_{\pi 2}}{r_{\pi 2} + (1 + \beta) R_{E 2}}$$

$$v_{\pi 2} = -g_m v_{\pi 1} R_{eq} \frac{r_{\pi 2}}{r_{\pi 2} + (1 + \beta) R_{E 2}} \longrightarrow \textcircled{1}$$

$$\therefore v_{\pi 1} = v_s \longrightarrow \textcircled{1}$$

$$v_{\pi 2} = -g_m v_s R_{eq} \frac{r_{\pi 2}}{r_{\pi 2} + (1 + \beta) R_{E 2}}$$

$$v_o = +g_m g_m v_s R_{eq} \frac{r_{\pi 2}}{r_{\pi 2} + (1 + \beta) R_{E 2}} R_{Ley}$$

