



Answer the following questions:

Q1: Complete the following sentences:

- i. is the boundary between p-type and n-type semiconductors in a diode.
- ii. The PIV is the maximum voltage appearing across the diode in
- iii. The output frequency of a half-wave rectifier the input frequency.
- iv. Diode cut off voltage above or below specified levels.
- v. The DC value of a half wave rectifier voltage with a peak sinusoidal value of 10V is
- vi. The ripple factor can be decreased by increasing the value of the
- vii. The operates in reverse breakdown region.
- viii. The term refers to two types of current: electron current and current.
- ix. The bias methods for discrete BJT circuit are using,, and
- x. A capacitor placed across the emitter resistor of CE amplifier is known as
- xi. In amplifier, the input and output voltages are 180° out of phase.
- xii. amplifier is known as an emitter-follower.

Q2: (a) Determine and sketch the output waveform for the network of Fig. (1).

- (b) The Si Darlington transistor pair of Fig.(2) has $\beta_1 = \beta_2 = 50$ and $R_2 = 100 \text{ k}\Omega$. Find the values of R_1 and V_{CE1} needed to bias the circuit so that $V_{CE2} = 6\text{V}$.

Q3: Consider the circuit shown in Figure (3). Let $V_S = 12 \text{ V}$, $V_{Z0} = 6.2 \text{ V}$, and $r_z = 3\Omega$. The maximum power rating of the diode is $P = 1 \text{ W}$.

- (a) Determine $I_Z(\text{max})$ and R_i for no load.
- (b) If $I_Z(\text{min}) = 0.1 I_Z(\text{max})$, determine $R_L(\text{min})$.

Q4: For the amplifier shown in Fig.(4), $\beta = 200$. (a) Determine the dc values of I_E and V_E .

- (b) Using the small signal hybrid π -model calculate the values of R_i , R_o , and the voltage gain (v_o/v_s).

Q5: Consider the ac equivalent circuit in Figure (5). The transistor parameters are $\beta_1 = 120$, $\beta_2 = 80$, $V_{A1} = V_{A2} = \infty$, and $I_{C1} = I_{C2} = 1 \text{ mA}$.

- (a) Calculate the input resistance R_i , and the output resistance R_o .
- (b) Find the small-signal voltage gain $A_{V1} = V_{o1}/V_i$.
- (c) Determine the small signal voltage gain $A_{V2} = V_{o2}/V_{o1}$.
- (d) Find the overall small-signal voltage gain $A_v = V_{o2}/V_i$.
- (e) Calculate the current gain $A_i = (i_o/i_s)$.

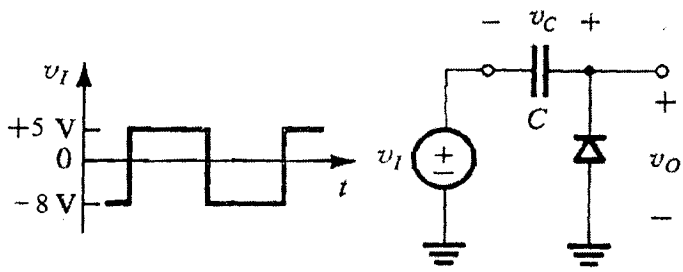


Fig.(1)

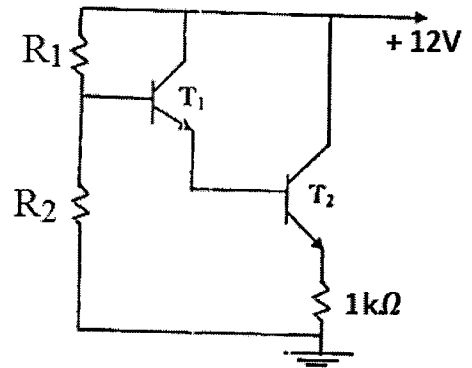


Fig.(2)

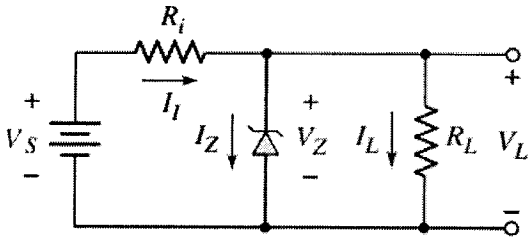


Fig.(3)

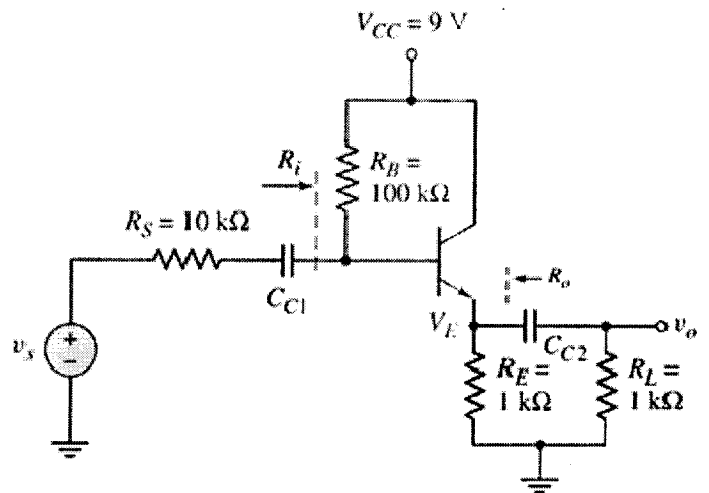


Fig.(4)

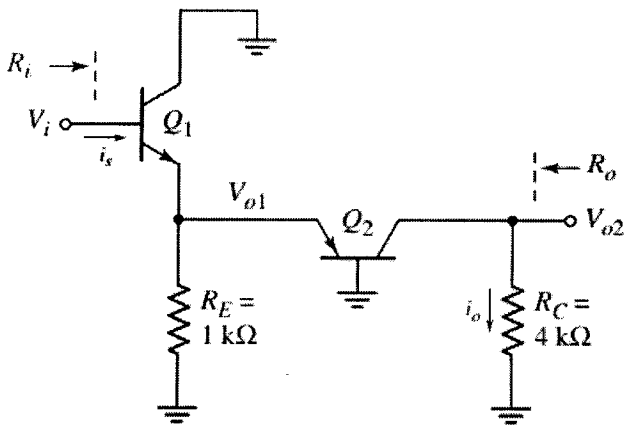


Fig.(5)

BEST WISHES

Hossam Labil



Answer the following questions:

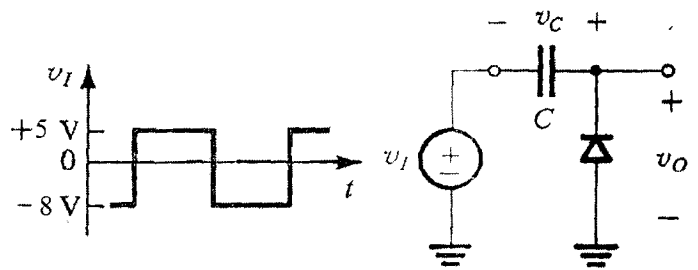
Q1: Complete the following sentences:

- i. A pn junction is the boundary between p-type and n-type semiconductors in a diode.
- ii. The PIV is the maximum voltage appearing across the diode in reverse bias.
- iii. The output frequency of a half-wave rectifier equals the input frequency.
- iv. Diode limiters cut off voltage above or below specified levels.
- v. The DC value of a half wave rectifier voltage with a peak sinusoidal value of 10V is $10/\pi=3.1831V$.
- vi. The ripple factor can be decreased by increasing the value of the filter capacitor.
- vii. The zener diode operates in reverse breakdown region.
- viii. The term bipolar refers to two types of current: electron current and hole current.
- ix. The bias methods for discrete BJT circuit are using single power supply (voltage divider bias), using two power supplies, and using a collector-to- base feedback resistor, OR using constant current source.
- x. A capacitor placed across the emitter resistor of CE amplifier is known as bypass capacitor.
- xi. In common emitter amplifier, the input and output voltages are 180 out of phase.
- xii. A common-collector amplifier is known as an emitter-follower.

Q2(a)

Determine and sketch the output waveform for the network of Fig. (1).

Solution:

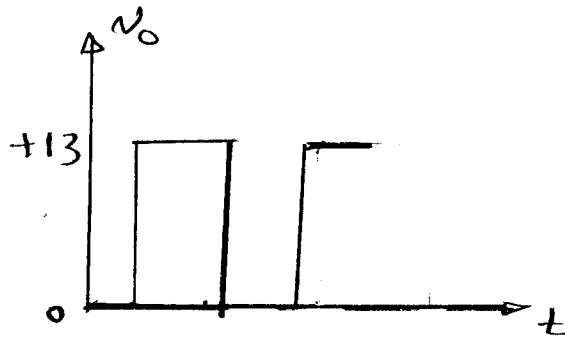


$$V_c = 8V$$

$$V_o = v_i + V_c$$

ie $V_o = v_i$ shifted by $-ve$ half cycle.

$$\therefore V_o = v_i + 8V$$



Q2 (b)

The Si Darlington transistor pair of Fig.(2) has $\beta_1 = \beta_2 = 50$ and $R_2 = 100 \text{ k}\Omega$. Find the values of R_1 , and V_{CE1} needed to bias the circuit so that $V_{CE2} = 6 \text{ V}$.

Solution:

$$V_{C1} = V_{C2} = V_{CC} = 12 \text{ V}$$

$$\therefore V_{CE2} = 6 \text{ V}$$

$$\therefore V_{CE2} = V_{C2} - V_{E2}$$

$$\therefore V_{E2} = V_{C2} - V_{CE2} \\ = 12 - 6 = 6 \text{ V}$$

$$I_{E2} = \frac{V_{E2}}{R_{E2}} = \frac{6}{1\text{K}} = 6 \text{ mA}$$

$$V_{B1} = V_{BE1} + V_{BE2} + V_{E2} \\ = 0.7 + 0.7 + 6 = 7.4 \text{ V}$$

$$I_2 = \frac{V_{B1}}{R_2} = \frac{7.4}{100\text{K}} = 74 \text{ }\mu\text{A}$$

$$I_{B2} = I_{E1} = \frac{I_{E2}}{1 + \beta_2} = \frac{6 \text{ mA}}{1 + 50} = 0.1176 \text{ mA}$$

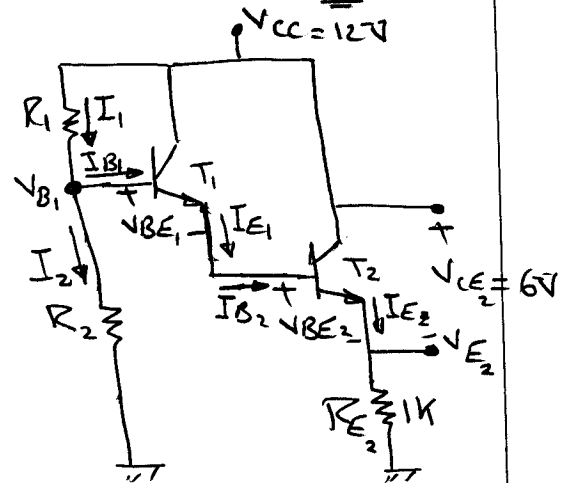
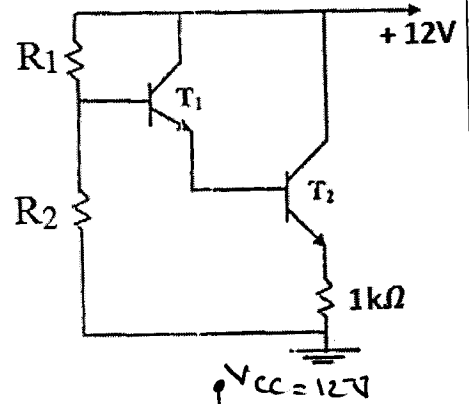
$$I_{B1} = \frac{I_{E1}}{1 + \beta_1} = \frac{0.1176 \text{ mA}}{51} = 2.306 \text{ }\mu\text{A}$$

$$\therefore I_1 = I_{B1} + I_2 = 2.306 \text{ }\mu\text{A} + 74 \text{ }\mu\text{A} = 76.306 \text{ }\mu\text{A}$$

$$R_1 = \frac{V_{CC} - V_{B1}}{I_1} \\ = \frac{12 - 7.4}{76.306 \text{ }\mu\text{A}} = 60.284 \text{ k}\Omega$$

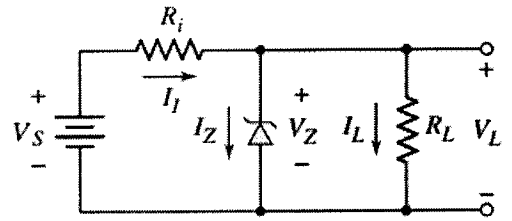
$$V_{E1} = V_{B1} - V_{BE1} \\ = 7.4 - 0.7 = 6.7 \text{ V}$$

$$\therefore V_{CE1} = V_{C1} - V_{E1} \\ = 12 - 6.7 = 5.3 \text{ V}$$



Q3

Consider the circuit shown in Figure (.). Let $V_S = 12\text{ V}$, $V_{Z0} = 6.2\text{ V}$, and $r_z = 3$. The maximum power rating of the diode is $P = 1\text{ W}$. (a) Determine $I_{Z(\max)}$ and R_i for no load. (b) If $I_{Z(\min)} = 0.1 I_{Z(\max)}$, determine $R_{L(\min)}$



Solution:

$V_S = 12\text{ V}$; $V_{Z0} = 6.2\text{ V}$; $r_z = 3\ \Omega$; $P_{Z\max} = 1\text{ W}$

(a) find $I_{Z\max}$ and R_i for no load

$$V_Z = V_{Z0} + I_Z r_z$$

$$V_Z = 6.2 + 3 I_Z \quad \text{--- (1)}$$

$$\therefore P_Z = I_Z V_Z$$

$$1 = I_Z (6.2 + 3 I_Z)$$

$$1 = 6.2 I_Z + 3 I_Z^2 \Rightarrow 3 I_Z^2 + 6.2 I_Z - 1 = 0$$

$$\therefore I_Z = \frac{-6.2 \pm \sqrt{(6.2)^2 + 4 \times 3 \times 1}}{2 \times 3} = -1.0333 \pm 1.1834$$

$$\therefore I_Z = -1.0333 + 1.1834 = 150\text{ mA}$$

$$\text{OR } I_Z = -1.0333 - 1.1834 = -2.217 \text{ (rejected)}$$

$$\therefore I_{Z|_{\max}} = 150\text{ mA} = I_I$$

$$V_Z = 6.2 + 3 \times 150\text{ m} = 6.65\text{ V} = V_L|_{\text{no load}}$$

$$R_i = \frac{V_S - V_Z}{I_I} = \frac{12 - 6.65}{150\text{ m}} = 35.7\ \Omega$$

(b) If $I_{Z\min} = 0.1 I_{Z\max}$ find $R_{L\min}$ and Load regulation.

$$I_{Z\min} = 0.1 \times 150\text{ m} = 15\text{ mA}$$

$$V_Z = V_L = V_{Z0} + I_{Z|_{\min}} r_z = 6.2 + 15\text{ m} \times 3 = 6.245\text{ V}$$

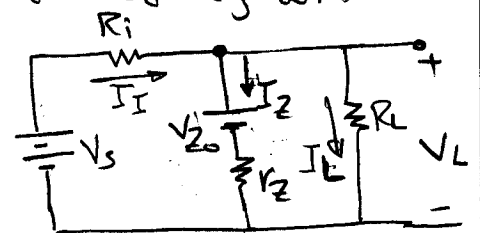
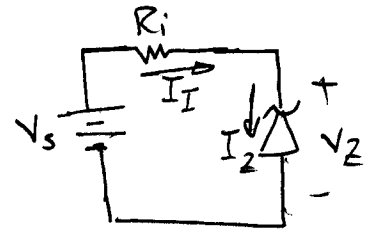
$$R_{L\min} = \frac{V_L}{I_L} = \frac{V_Z}{I_L}$$

$$\therefore I_L = I_I - I_{Z|_{\min}}$$

$$\therefore I_I = \frac{V_S - V_Z}{R_i} = \frac{12 - 6.245}{35.7} = 161.2\text{ mA}$$

$$\therefore I_L = 161.2\text{ m} - 15\text{ m} = 146.2\text{ mA}$$

$$\therefore R_{L\min} = \frac{6.245}{146.2\text{ m}} = 42.7\ \Omega$$



Q4

For the amplifier shown in Fig.(4), $\beta = 200$.

(a) Determine the dc values of I_E and V_E .

(b) Using the small signal hybrid π -model calculate the values of R_i , R_o , and the voltage gain (v_o/v_s).

Solution:

DC Analysis

- ALL capacitors are o.c
- Reduce AC sources

Loop (I)

$$-V_{CC} + I_B R_B + V_{BE} + I_E R_E = 0$$

$$\therefore I_B = \frac{I_E}{1+\beta}$$

$$-V_{CC} + \frac{I_E}{1+\beta} R_B + V_{BE} + I_E R_E = 0$$

$$-V_{CC} + I_E \left(\frac{R_B}{1+\beta} + R_E \right) + V_{BE} = 0$$

$$I_E = \frac{V_{CC} - V_{BE}}{\frac{R_B}{1+\beta} + R_E} = \frac{9 - 0.7}{\frac{100k}{201} + 1k} = 5.543 \text{ mA}$$

$$V_E = I_E R_E = 5.543 \text{ mA} \times 1k = 5.543 \text{ V}$$

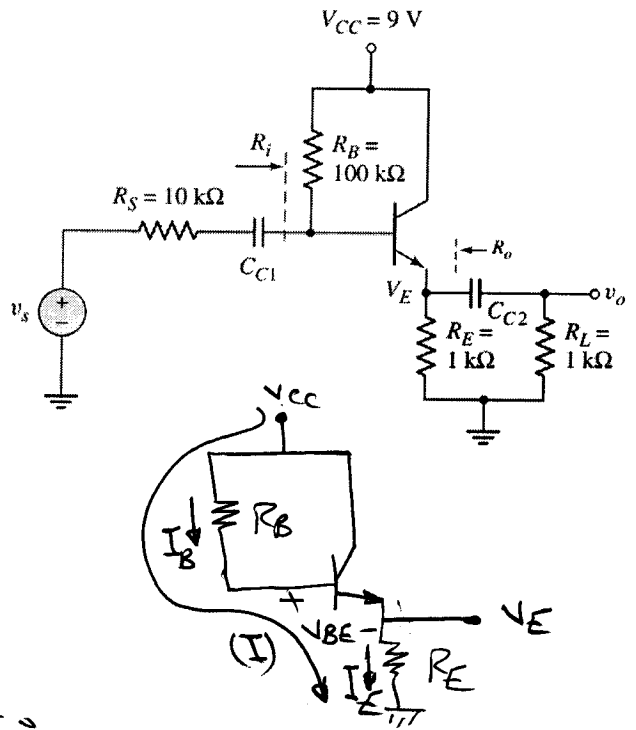
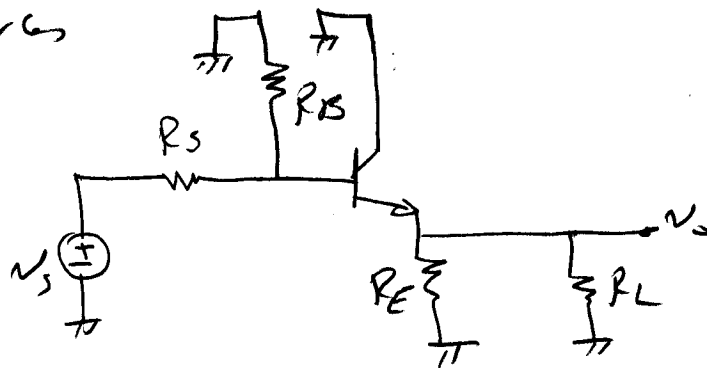
$$I_C = \alpha I_E = \frac{200}{201} \times 5.543 \text{ mA} = 5.515 \text{ mA}$$

$$g_m = \frac{I_C}{V_T} = \frac{5.515 \text{ mA}}{25 \text{ mV}} = 220.6 \text{ mA/V}$$

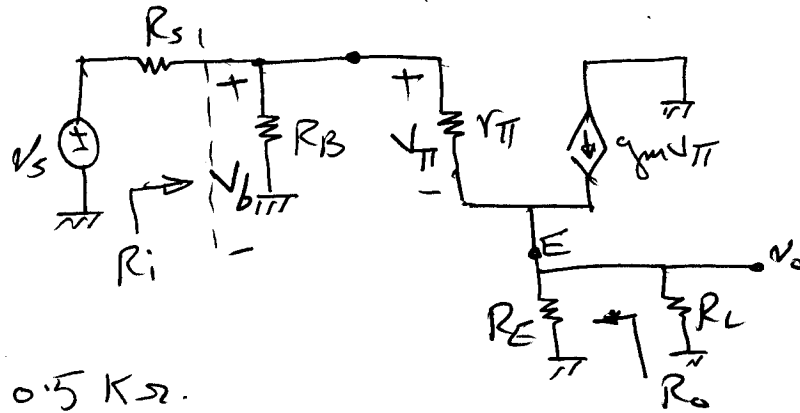
$$r_{\pi} = \frac{\beta}{g_m} = \frac{200}{220.6} = 906.62 \Omega$$

AC Analysis

- ALL capacitors are s.c
- Reduce DC sources



Q4 (cont.)



$$R_L' = R_E \parallel R_L$$

$$= 1\text{K} \parallel 1\text{K} = 0.5\text{K}\Omega$$

$$R_i = R_B \parallel [r_{\pi} + (1+\beta)R_L']$$

$$= 100\text{K} \parallel [906.62 + (1+200) \times 0.5\text{K}]$$

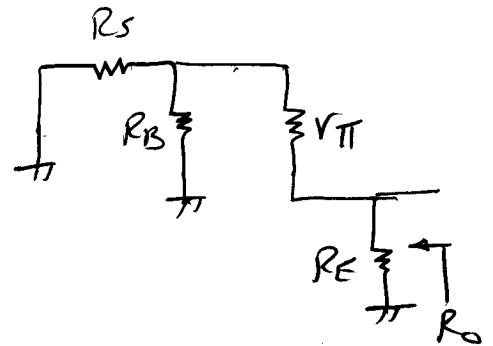
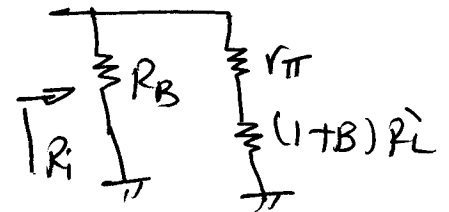
$$= 100\text{K} \parallel 101.41\text{K} = 50.35\text{K}\Omega$$

$$R_o = \left[\frac{(R_s \parallel R_B + r_{\pi})}{1+\beta} \right] \parallel R_E$$

$$v_s = 0$$

$$= \left[\frac{(100\text{K} \parallel 100\text{K}) + 906.62}{201} \right] \parallel 1\text{K}$$

$$= 49.74 \parallel 1\text{K} = 47.38\Omega$$



To find $A_v = \frac{v_o}{v_s}$

$$v_b = \frac{v_s R_i}{R_i + R_s}$$

$$v_o = v_b \frac{(1+\beta)R_L'}{r_{\pi} + (1+\beta)R_L'} = \frac{v_s R_i}{R_i + R_s} \times \frac{(1+\beta)R_L'}{r_{\pi} + (1+\beta)R_L'}$$

$$\therefore A_v = \frac{v_o}{v_s} = \frac{R_i}{R_i + R_s} \frac{(1+\beta)R_L'}{r_{\pi} + (1+\beta)R_L'}$$

$$= \frac{50.35\text{K}}{50.35\text{K} + 100\text{K}} \frac{201 \times 0.5\text{K}}{906.62 + 201 \times 0.5\text{K}}$$

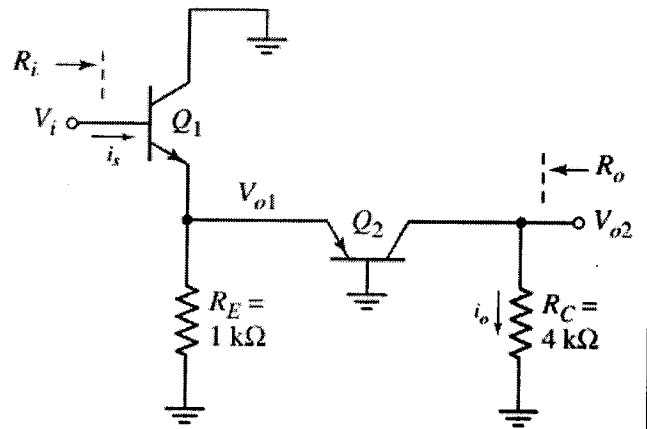
$$= 1.002 \times 0.9911 = 0.993 \text{ V/V}$$

Q5

Consider the ac equivalent circuit in Figure (5).

The transistor parameters are $\beta_1 = 120$, $\beta_2 = 80$, $V_{A1} = V_{A2} = \infty$, and $I_{C1} = I_{C2} = 1 \text{ mA}$.

- Calculate the input resistance R_i , and the output resistance R_o .
- Find the small-signal voltage gain $A_{V1} = V_{o1}/V_i$.
- Determine the small signal voltage gain $A_{V2} = V_{o2}/V_{o1}$.
- Find the overall small-signal voltage gain $A_v = V_{o2}/V_i$.
- Calculate the current gain $A_i = (i_o/i_s)$.



Solution:

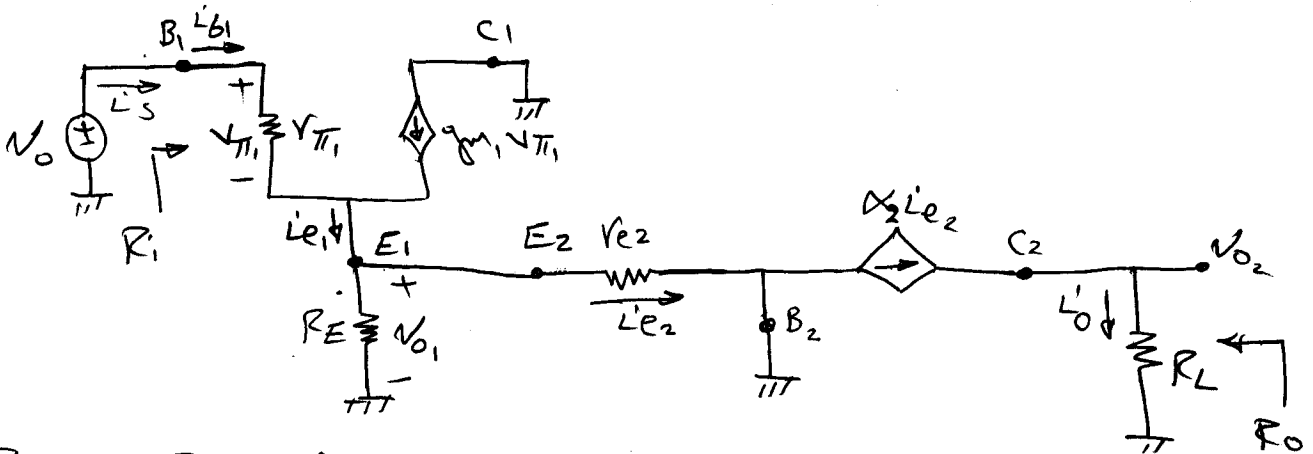
$$\therefore I_{C1} = I_{C2} = 1 \text{ mA} = I_C \text{ (given)}$$

$$\therefore g_{m1} = g_{m2} = \frac{I_C}{V_T} = \frac{1 \text{ m}}{25 \text{ m}} = 40 \text{ mA/V}$$

$$r_{\pi 1} = \frac{\beta_1}{g_{m1}} = \frac{120}{40 \text{ m}} = 3 \text{ k}\Omega$$

$$r_{e2} = \frac{\alpha_2}{g_{m2}} \approx \frac{1}{g_{m2}} = \frac{1}{40 \text{ m}} = 25 \Omega$$

Ac Analysis



$$(a) R_{ET} = R_E \parallel r_{e2} = 1 \text{ k} \parallel 25 = 24.39 \Omega$$

$$R_i = r_{\pi 1} + (1 + \beta_1) R_{ET}$$

$$= 3 \text{ k} + (1 + 120) * 24.39 = 5.95 \text{ k}\Omega$$

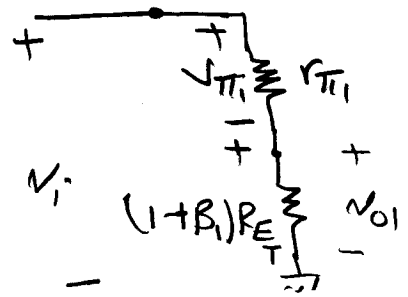
$$R_o|_{V_i=0} = R_C = 4 \text{ k}\Omega$$

Q5(cont.)

(b) To find $A_{V1} = \frac{V_{o1}}{V_i}$

$$V_{o1} = V_i \frac{(1+\beta_1) R_{ET}}{r_{\pi_1} + (1+\beta_1) R_{ET}}$$

$$\begin{aligned} \therefore A_{V1} &= \frac{V_{o1}}{V_i} = \frac{(1+\beta_1) R_{ET}}{r_{\pi_1} + (1+\beta_1) R_{ET}} \\ &= \frac{(1+120) * 24.39}{3K + 121 * 24.39} = 0.496 \text{ V/V} \end{aligned}$$



(c) To find $A_{V2} = \frac{V_{o2}}{V_{o1}}$

$$V_{o2} = \alpha_2 I_{e2} R_C$$

$$I_{e2} = \frac{V_{o1}}{r_{e2}}$$

$$\therefore V_{o2} = \alpha_2 \frac{V_{o1}}{r_{e2}} R_C$$

$$\therefore A_{V2} = \frac{V_{o2}}{V_{o1}} = \frac{\alpha_2 R_C}{r_{e2}} = g_{m2} R_C$$

$$= 40M * 4K = 160 \text{ V/V}$$

$$(d) A_V = \frac{V_{o2}}{V_i} = \frac{V_{o1}}{V_i} * \frac{V_{o2}}{V_{o1}} = A_{V1} * A_{V2}$$

$$= 0.496 * 160 = 79.36 \text{ V/V}$$

(e) To find $A_i = \frac{I_o}{I_s}$

$$I_o = \alpha_2 I_{e2}$$

$$I_{e2} = I_{e1} \frac{R_E}{R_E + r_{e2}} \quad ; \quad I_{e1} = (1+\beta_1) I_{b1}$$

$$\therefore I_{b1} = I_s \Rightarrow I_{e1} = (1+\beta_1) I_s$$

$$\therefore I_{e2} = (1+\beta_1) I_s \frac{R_E}{R_E + r_{e2}}$$

$$\therefore I_o = \alpha_2 (1+\beta_1) I_s \frac{R_E}{R_E + r_{e2}}$$

$$\therefore A_i = \frac{I_o}{I_s} = \alpha_2 (1+\beta_1) \frac{R_E}{R_E + r_{e2}}$$

$$= 1 * 121 \frac{1K}{1K + 25} = 118.05 \text{ A/A}$$